Applications of Non-Intrusive Load Monitoring (NILM) to Power Systems and New NILM-type Problems

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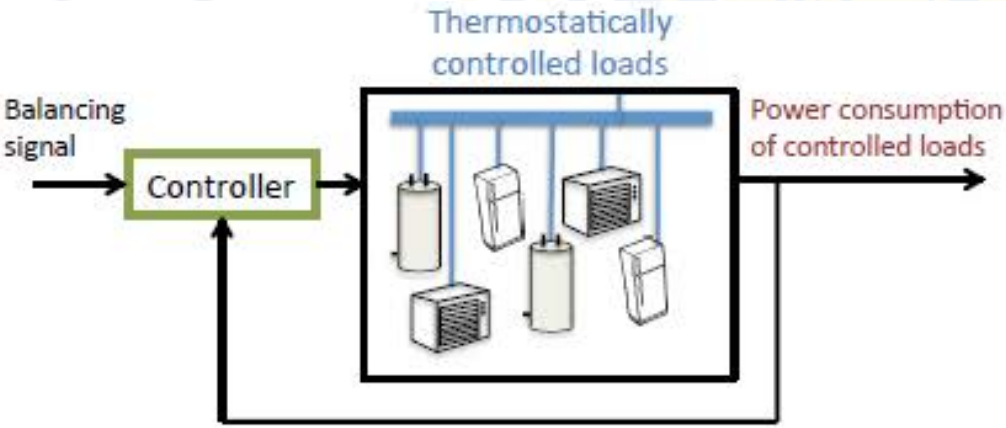
Disclaimer

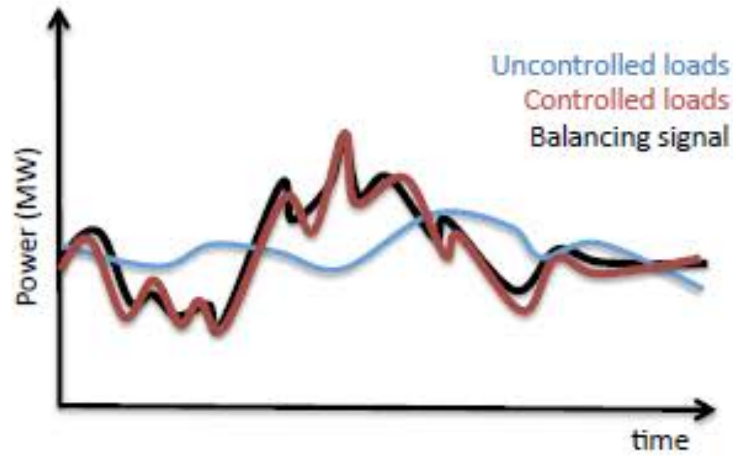
- I'm not an NILM expert. My primary field is electric power systems.
- I first learned about NILM from Mario when he visited Berkeley Lab in 2011!
- …but I do think a lot about electric loads, specifically, how to harvest flexibility from loads (residential, commercial, industrial, water…) to help the grid.

- Thanks for inviting me to give this keynote!

Harvesting Flexibility from Residential Loads

→ Load Aggregation and Coordination

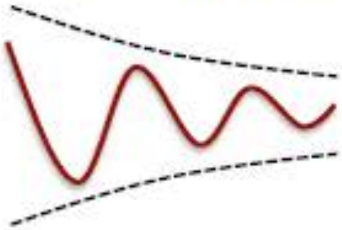




Network-Aware

Communication-Constrained

Stability Guarantees



ARPA-E Open 2018 Project

How is this connected to NILM?

- To solve load coordination problems we need models of loads and real-time feedback from loads (i.e., offline and online data).
- Smart meters now are pervasive but home energy management systems and submetering are not (and expensive).

  → NILM?

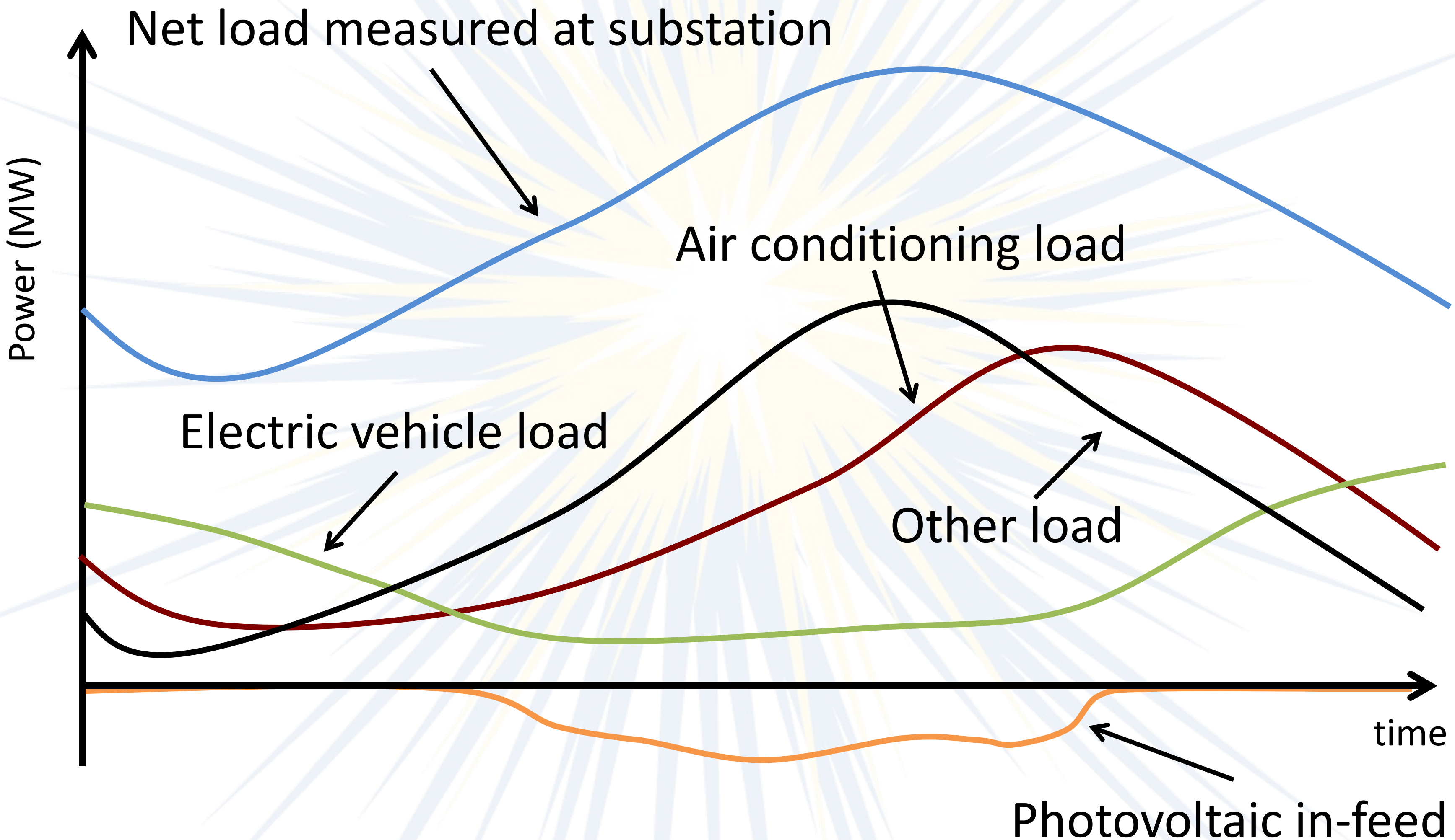
Applications of NILM in Power Systems

- Developing dynamical models of loads to better represent load in planning studies, and to use in grid operational strategies
- Estimating the availability/flexibility of responsive loads for demand response [He et al 2013, Yue et al 2020]
- Verifying load response after demand response events
- Real-time feedback on load response to improve demand response/grid services [Adabi et al 2016]

New NILM-type Problems

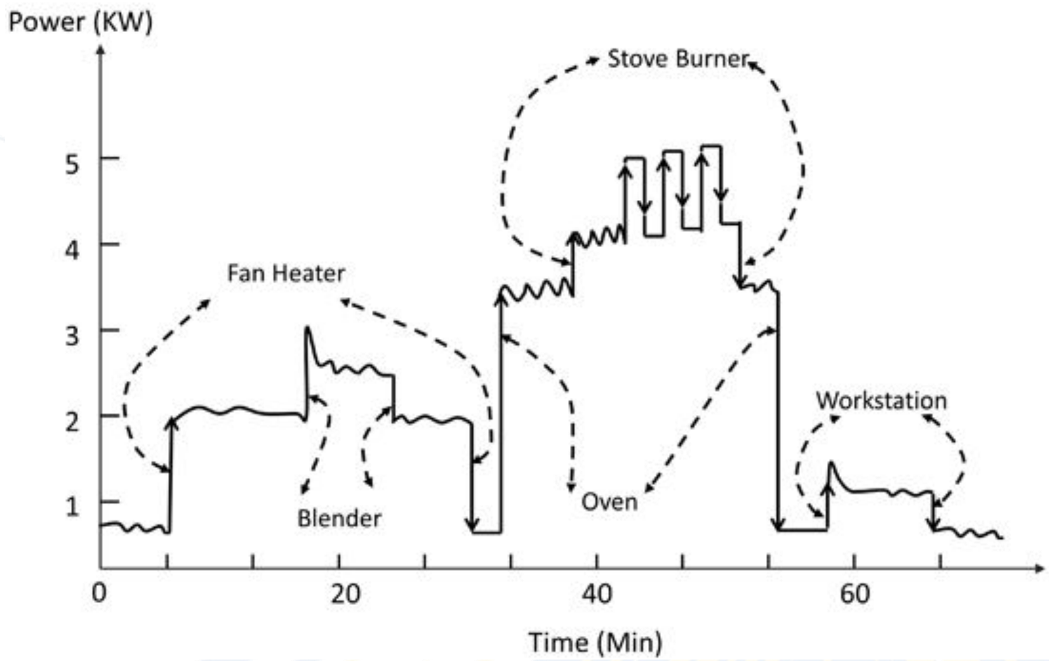
- Example: Disaggregating at points other than the household smart meter
- Significant recent interested in estimating solar PV generation (negative load) using feeder measurements [Kara et al 2018, Sossan et al 2018, Li et al 2019, Vrettos et al 2019,…]
- Disaggregation feeder load by type…

Feeder Energy Disaggregation



Energy Disaggregation

a.k.a Non-Intrusive Load Monitoring (NILM)



[Hart 2010; Ziefman and Roth 2011; Berges et al. 2009; Dong, Sastry, et al. 2013, 2014; Wytock & Kolter 2013; Kolter and Jaakkola 2012; Kim et al. 2010; …]

Fig from Zoha et al. 2012

Problem: Estimate individual load from a single power measurement (usually) sampled at high frequency (10kHz-1MHz) from the household main

Solution approaches: offline algorithms including change detection, supervised learning, unsupervised learning

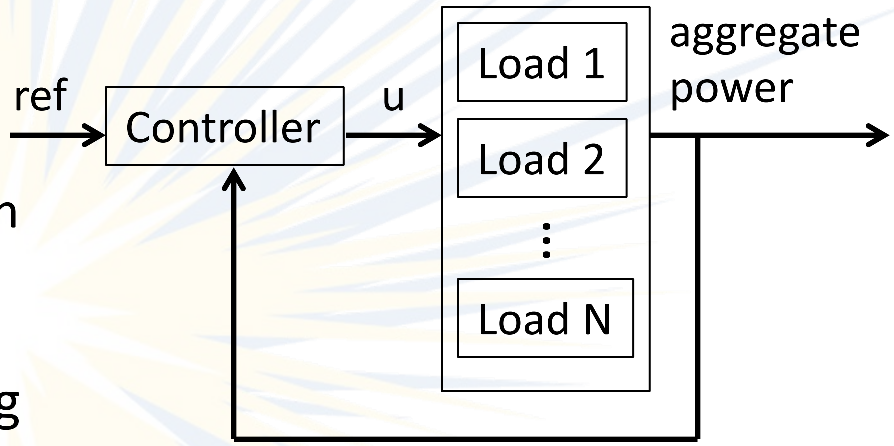
Key Differences

- We assume measurements at the substation, not the household
- We estimate the power consumption of all loads of a specific type, not individual loads
- We solve the problem online, not offline
- We use lower frequency measurements (e.g., taken every second to minute)
- In some cases, we may get to be "intrusive," but not in this talk!

Why disaggregate feeder load?

Uses in demand response…

- Load control feedback [noisy aggregate power measurements are assumed in Mathieu et al. 2013; Can Kara et al. 2013; Bušić and Meyn 2016; Callaway 2009; …]
- Load aggregator bidding
- Demand response event signaling (when/how much)



Beyond demand response…

- Energy efficiency via conservation voltage reduction (disaggregate by ZIP load type)
- Contingency planning (disaggregate motor loads)
- Reserve planning (disaggregate PV production)

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Possible Methods

- Short-term load (component) forecasting
  - Doesn't incorporate real-time feedback
- State estimation
  - Linear techniques require linear system models
  - Nonlinear techniques can be computationally demanding
- Online learning
  - (Typically) data-driven, model-free
- Hybrid approach: Dynamic Fixed Share & Dynamic Mirror Descent [Hall & Willet 2015]
  - Admits dynamic models of arbitrary forms
  - Optimization-based method to choose a weighted combination of the estimates of a collection of models

Outline

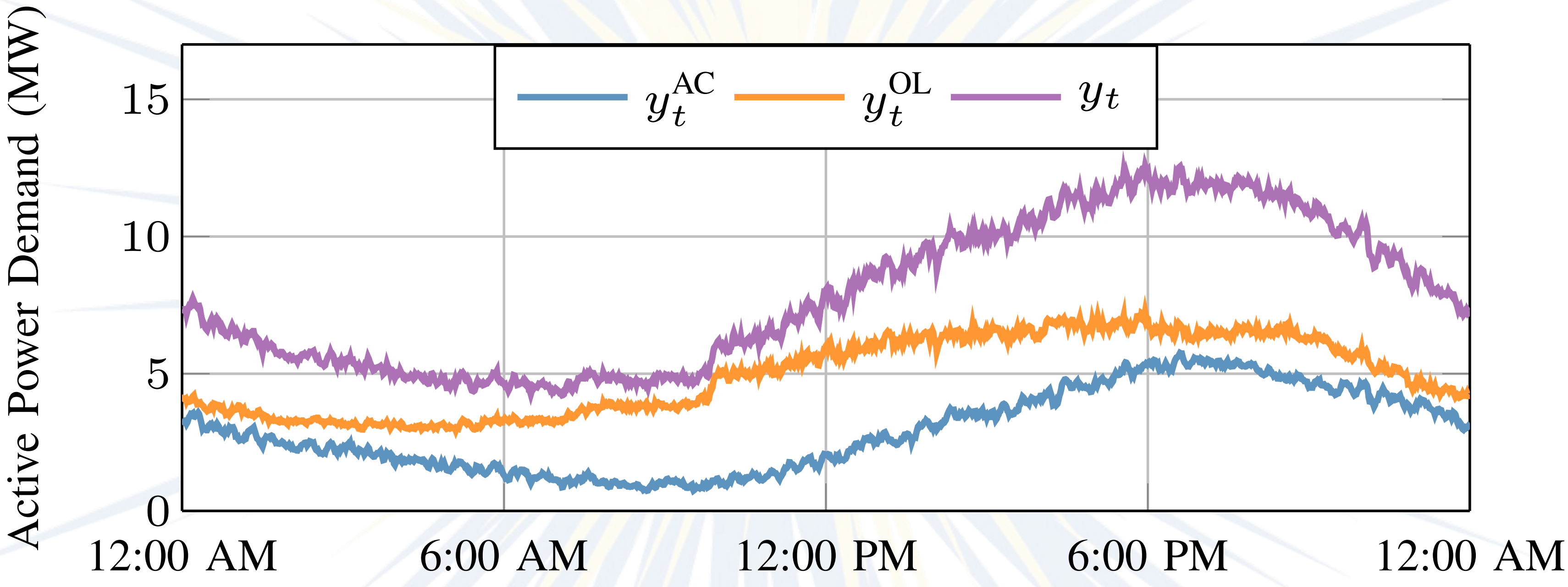
- Problem Framework
- Algorithms: Dynamic Mirror Descent (DMD) & Dynamic Fixed Share (DFS)
- Models, Algorithm Modifications
- Case studies
- Connections with Kalman Filtering
- Extension to multiple measurements

Ledva, Balzano, and Mathieu, “Inferring the Behavior of Distributed Energy Resources with Online Learning,” Allerton 2015.

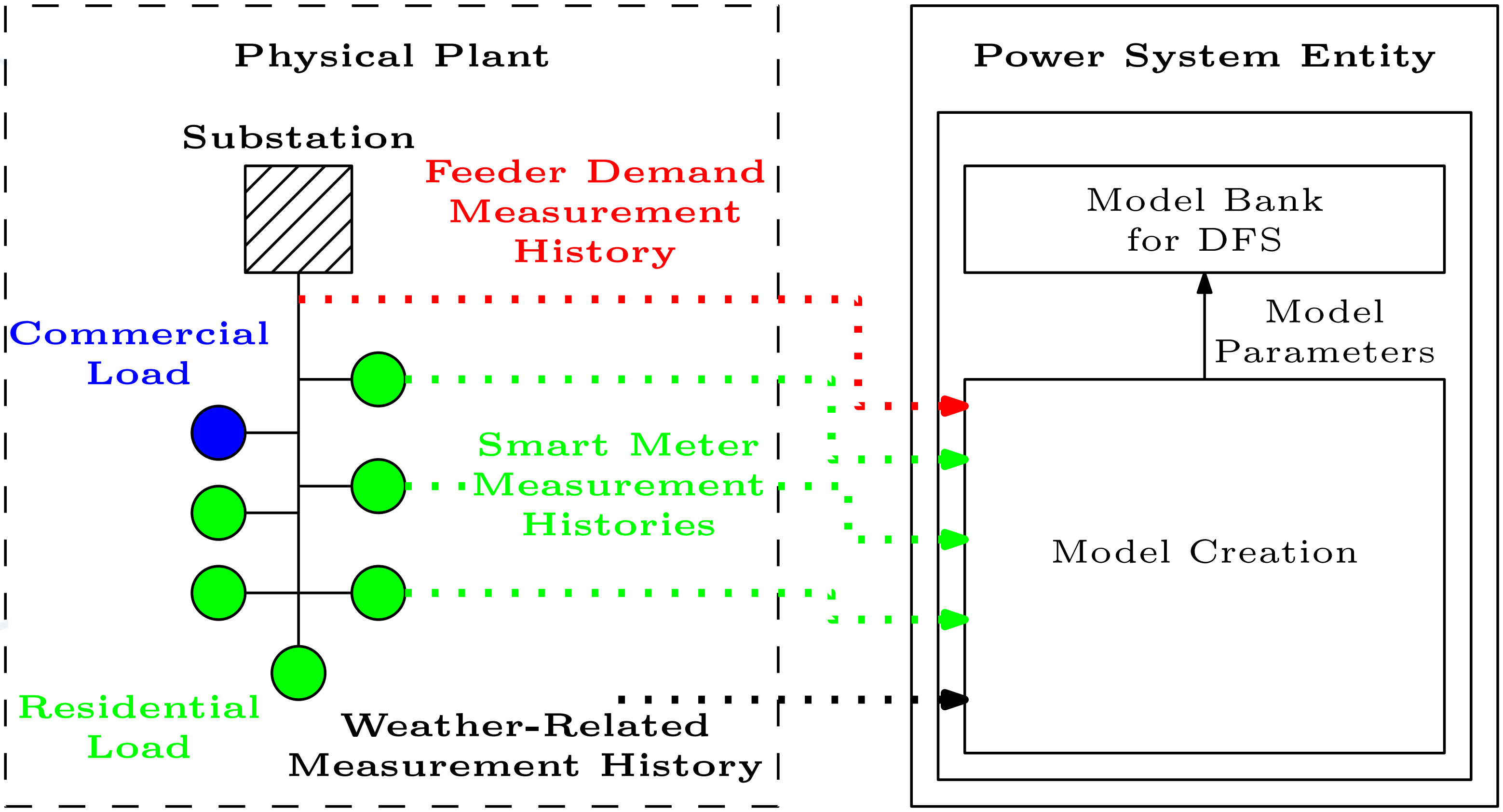
Ledva, Balzano, and Mathieu, “Real-time Energy Disaggregation of a Distribution Feeder’s Demand using Online Learning,” IEEE Transactions on Power Systems, 2018.

Problem Framework

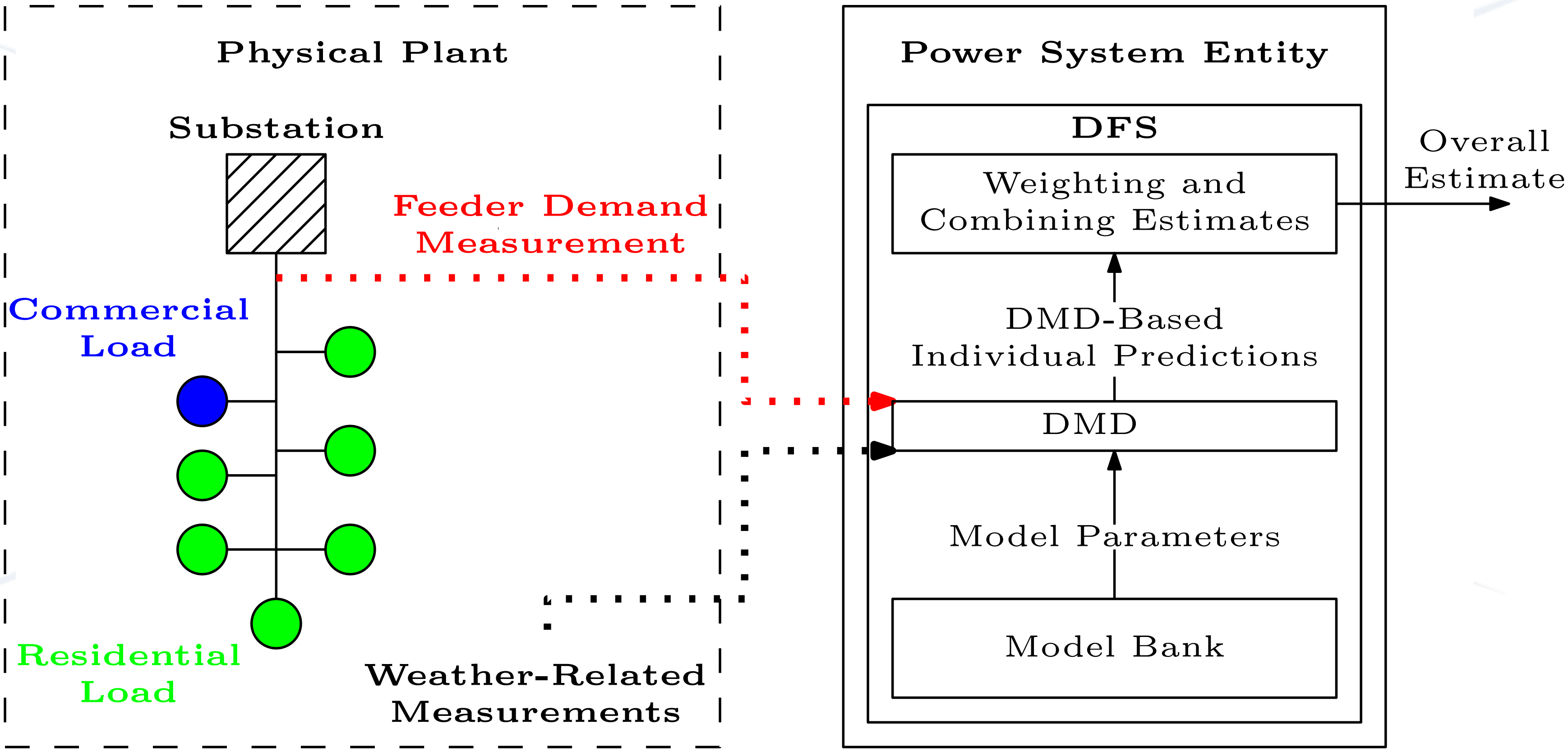
Measure the purple, Estimate the blue



Problem Framework: Offline Model Generation



Problem Framework: Real-time Estimation



DMD = Dynamic Mirror Descent, DFS = Dynamic Fixed Share

Dynamic Mirror Descent

[Hall & Willet 2015]

For each model m we compute

1. an observation-based update

$$\widetilde{\theta}_t^m = \arg\min_{\theta \in \Theta} \eta^s \left\langle \nabla \ell_t(\widehat{\theta}_t^m),\ \theta \right\rangle + D\left(\theta \| \widehat{\theta}_t^m\right)$$

   where $\ell_t(\widehat{\theta}_t^m)$ is a convex loss function and D is a Bregman divergence function

2. a model-based update

$$\widehat{\theta}_{t+1}^m = \Phi^m(\widetilde{\theta}_t^m)$$

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Dynamic Fixed Share

[Hall & Willet 2015]

3. Next, we update the weight of each model

$$w_{t+1}^{m} = \frac{\lambda}{N^{\mathrm{mdl}}} + (1-\lambda)\frac{w_t^m \ \exp\left(-\eta^r \, \ell_t\left(\widehat{\theta}_t^m\right)\right)}{\sum_{j=1}^{N^{\mathrm{mdl}}} w_t^j \ \exp\left(-\eta^r \, \ell_t\left(\widehat{\theta}_t^j\right)\right)}$$

4. and compute the overall estimate.

$$\widehat{\theta}_{t+1} = \sum_{m \in \mathcal{M}^{\mathrm{mdl}}} w_{t+1}^m \ \widehat{\theta}_{t+1}^m$$

Algorithmic Guarantees

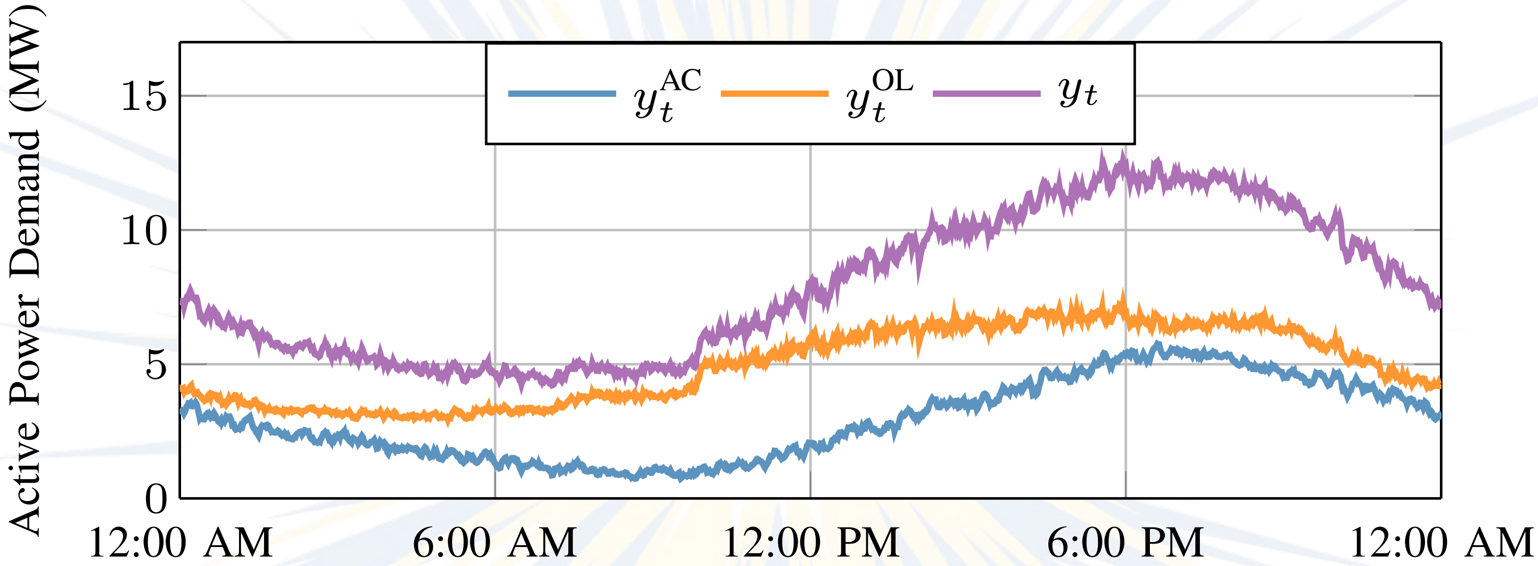
- Regret: performance with respect to a comparator $\boldsymbol{\theta}_T$

$$R_T(\boldsymbol{\theta}_T) \triangleq \sum_{t=1}^{T} \ell_t(\widehat{\theta}_t) - \sum_{t=1}^{T} \ell_t(\theta_t).$$

- Often the comparator is the performance of a batch algorithm

- Hall and Willet derive bounds on the regret and show that for many classes of comparators regret scales sublinearly in T

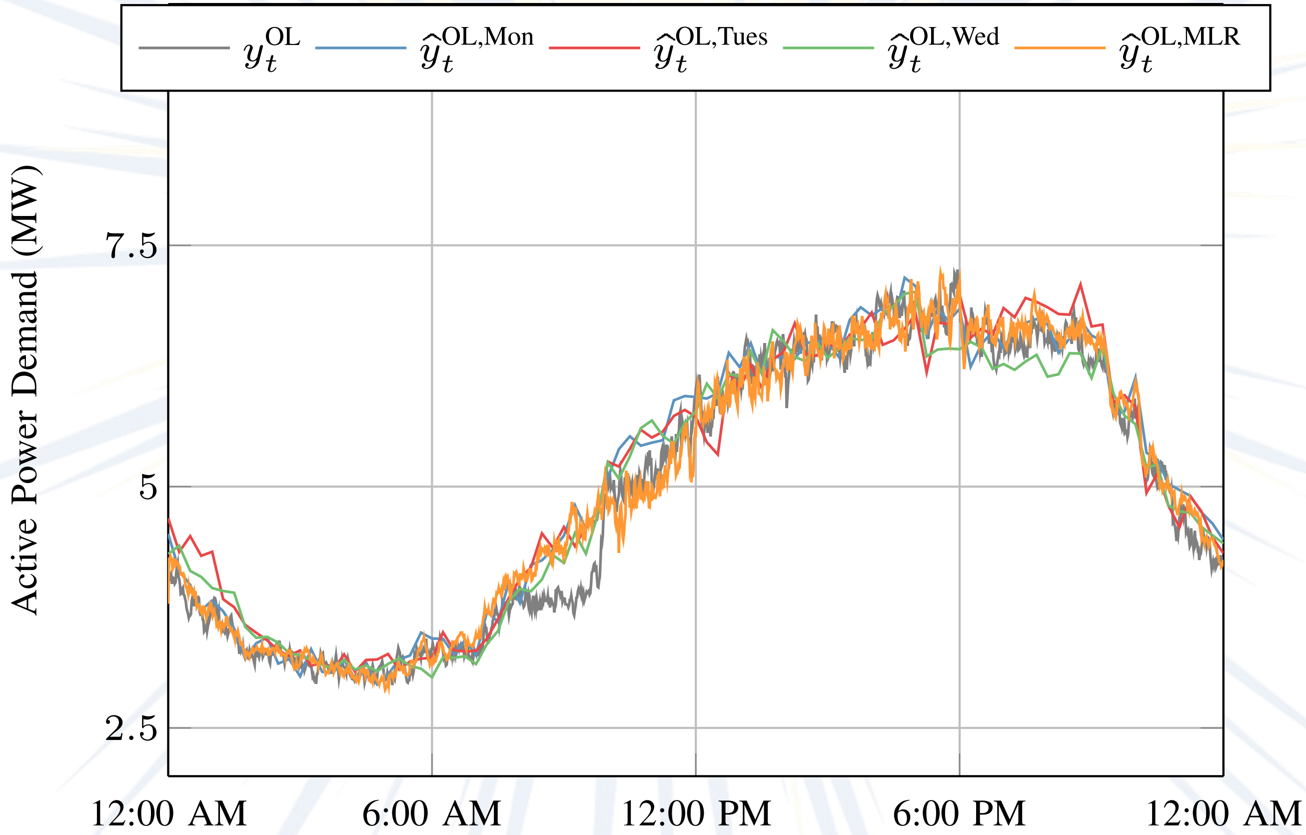
Models



- 29 aggregate air conditioning load (AC) models
- 6 "other load" (OL) model
- 1 AC model + 1 OL model = 1 total load model
  → 174 total load models

"Other load" Models

- (Smoothed) load on previous days (Mon-Fri)
- Multiple linear regression (MLR) model using time-of-week, outdoor temperature, and previous total demand measurement



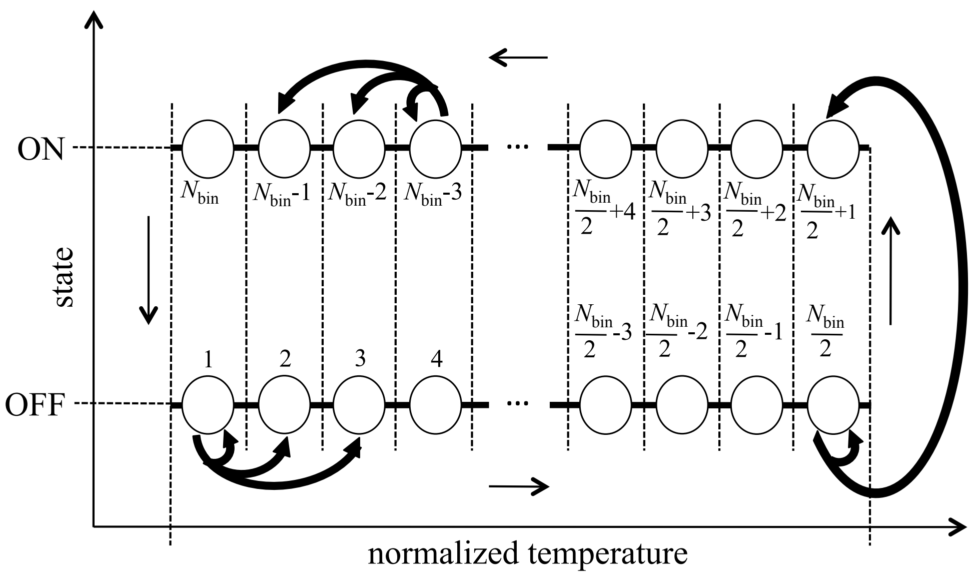
AC Models

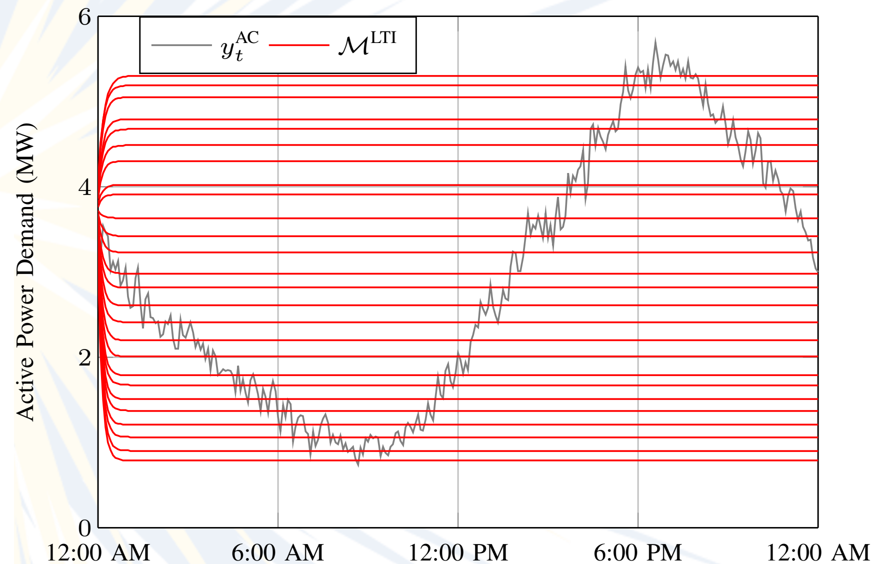
- Multiple linear regression (MLR) model using time-of-week and current/past outdoor temperatures
- Linear time-invariant (LTI) system models corresponding to different outdoor temperatures
- Linear time-varying (LTV) system models

Linear Time Invariant (LTI) Aggregate AC Model

[Mathieu et al. 2013]

$$\widehat{x}_{t+1}^{\mathrm{LTI},m} = A^{\mathrm{LTI},m}\ \widehat{x}_t^{\mathrm{LTI},m}$$
$$\widehat{y}_t^{\mathrm{AC,LTI},m} = C^{\mathrm{LTI},m}\ \widehat{x}_t^{\mathrm{LTI},m}$$



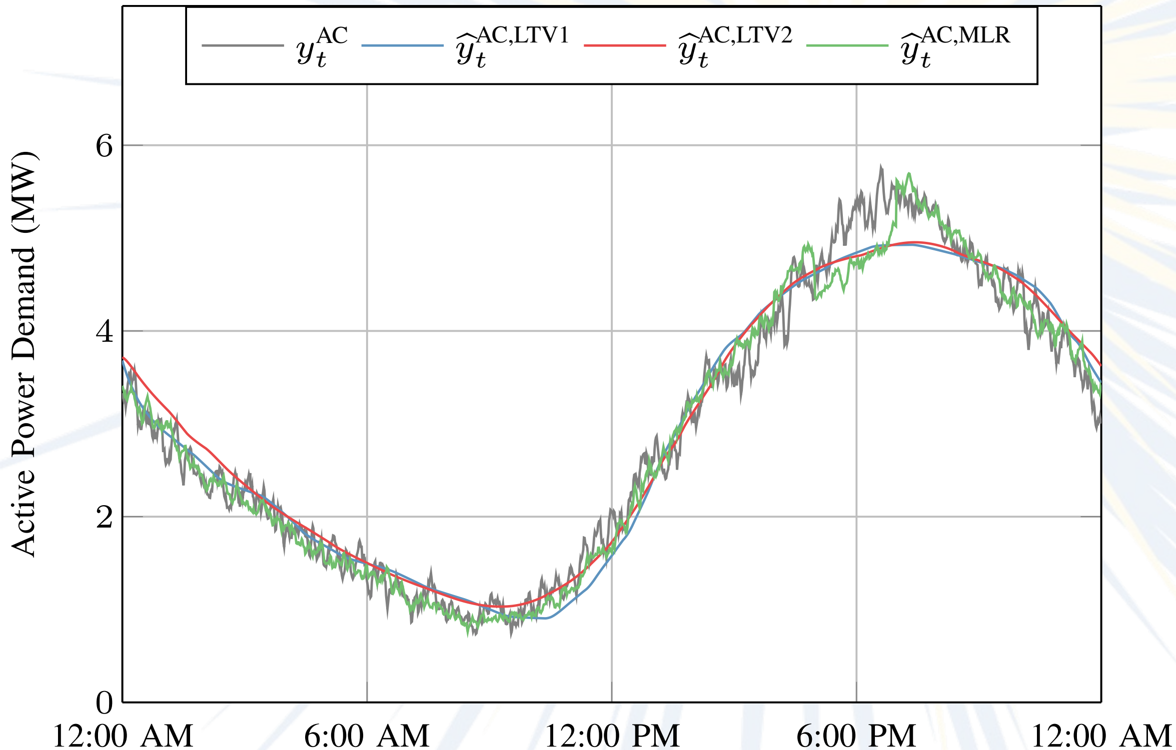


Linear Time Varying Aggregate AC Model

[Mathieu et al. 2015]

$$\widehat{x}_{t+1}^{\text{LTV1}} = A_t^{\text{LTV1}} \; \widehat{x}_t^{\text{LTV1}}$$

$$\widehat{y}_t^{\text{AC,LTV1}} = C_t^{\text{LTV1}} \; \widehat{x}_t^{\text{LTV1}}$$



Can identify A_t using delayed temperature measurements or a moving average of past temperature measurements

Algorithm Modifications

- The models have different structures, dynamic states, and/or parameters. It is difficult to define a common "state" θ_t .

- Two versions
  - Update Method 1: updates the output
  - Update Method 2: updates the state (i.e., for the LTI/LTV models, update the state, i.e., $\theta_t = x_t$)

Update Method 1

Adjust the output (demand estimates), rather than the state.

$$\widetilde{\theta}_t^m = \arg\min_{\theta\in\Theta} \eta^{\mathrm{s}} \left\langle \nabla \ell_t(\widehat{\theta}_t^m),\ \theta \right\rangle + D\left(\theta \| \widehat{\theta}_t^m\right)$$
$$\widehat{\theta}_{t+1}^m = \Phi^m(\widetilde{\theta}_t^m)$$

$$\widehat{\kappa}_{t+1} = \arg\min_{\theta\in\Theta} \eta^{\mathrm{s}} \left\langle \nabla \ell_t(\widehat{\theta}_t),\ \theta \right\rangle + D\left(\theta \| \widehat{\kappa}_t\right)$$
$$\check{\theta}_{t+1} = \Phi(\check{\theta}_t)$$
$$\widehat{\theta}_{t+1} = \check{\theta}_{t+1} + \widehat{\kappa}_{t+1}.$$

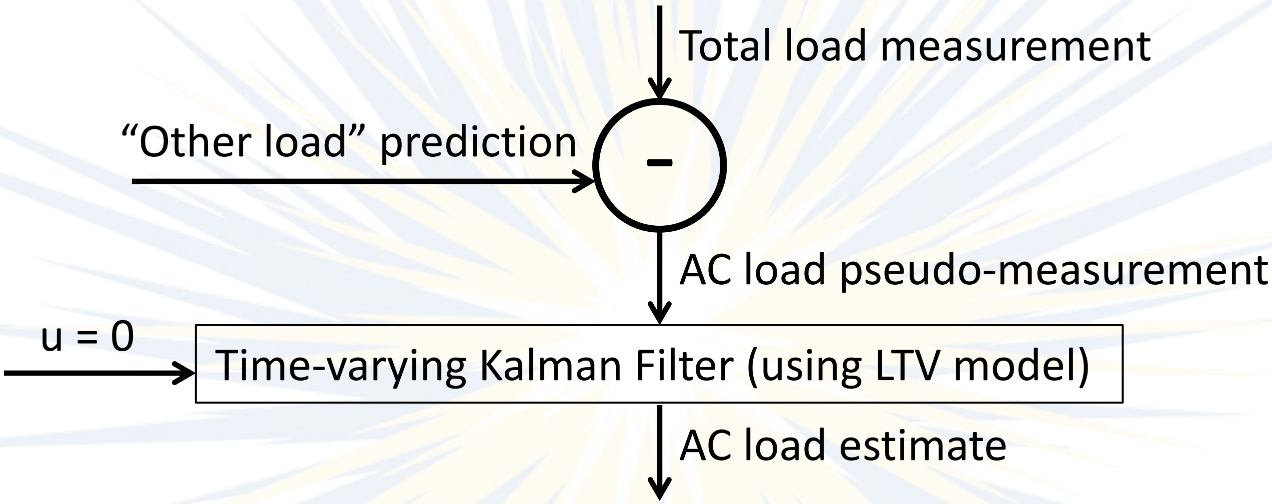
Then, with $\ell_t(\widehat{\theta}_t) = \frac{1}{2}\|C_t\widehat{\theta}_t - y_t\|_2^2$ and $D(\theta\|\widehat{\kappa}_t) = \frac{1}{2}\|\theta - \widehat{\kappa}_t\|_2^2$ we can derive a closed-form update:

$$\widehat{\kappa}_{t+1} = \widehat{\kappa}_t + \eta^{\mathrm{s}} C_t^T \left(y_t - C_t\widehat{\theta}_t\right)$$

Case studies: Plant

- Residential load and weather data from Pecan Street Dataport (Austin, TX)
- Commercial load data from Pacific Gas & Electric Company; weather data from NOAA (Bay Area, CA)
- GridLab-D feeder used to size the load

Case studies: Benchmark

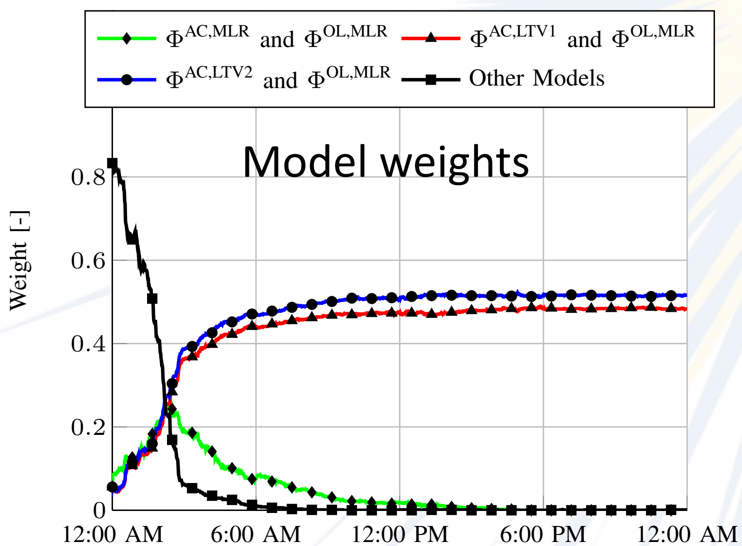


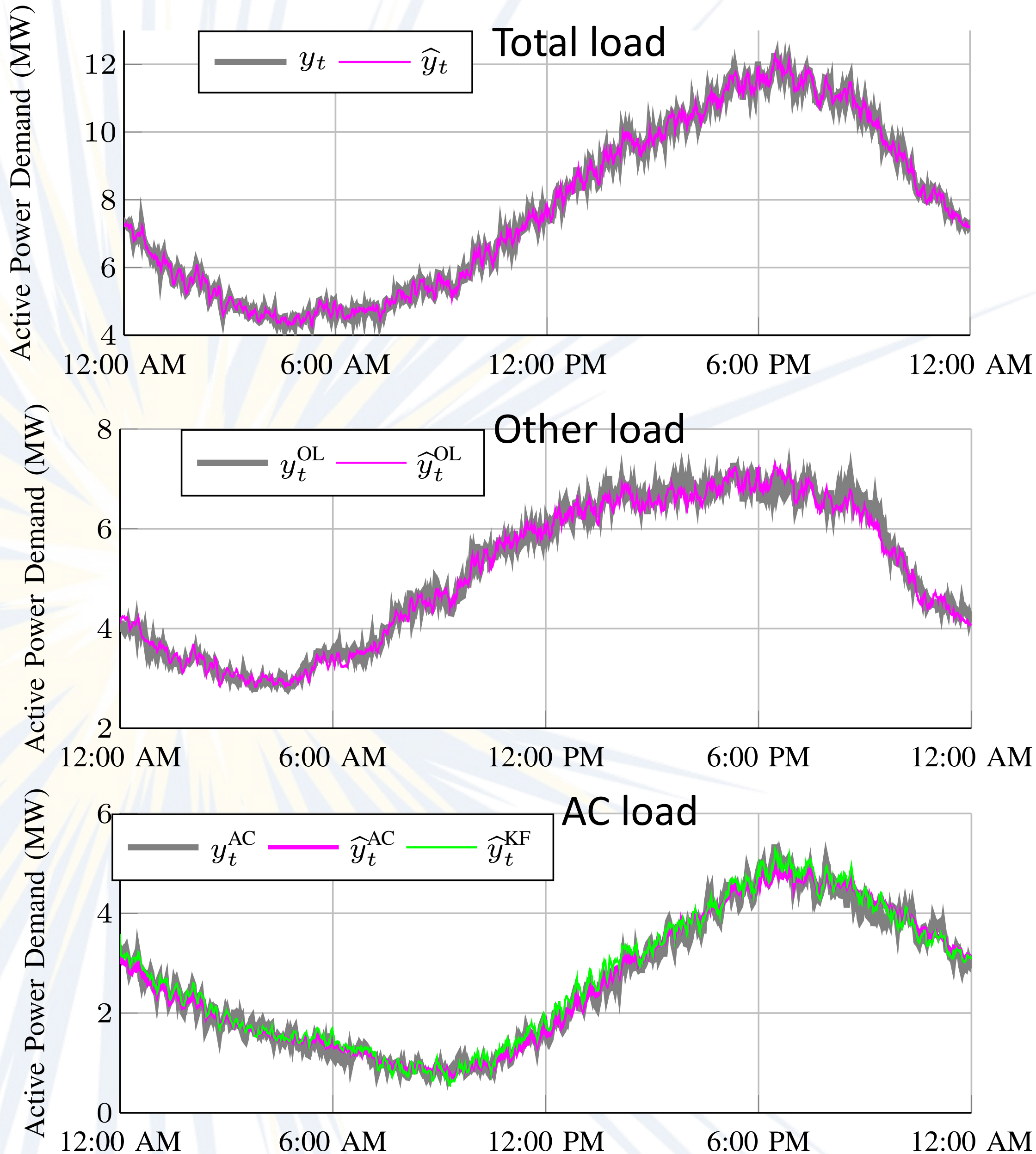
- Each “other load” model + LTV AC model combination is used to compute one AC load estimate.
- We obtain the estimates from all Kalman filters and compute the a posteriori best (BKF) and average (AKF) results.

Example results

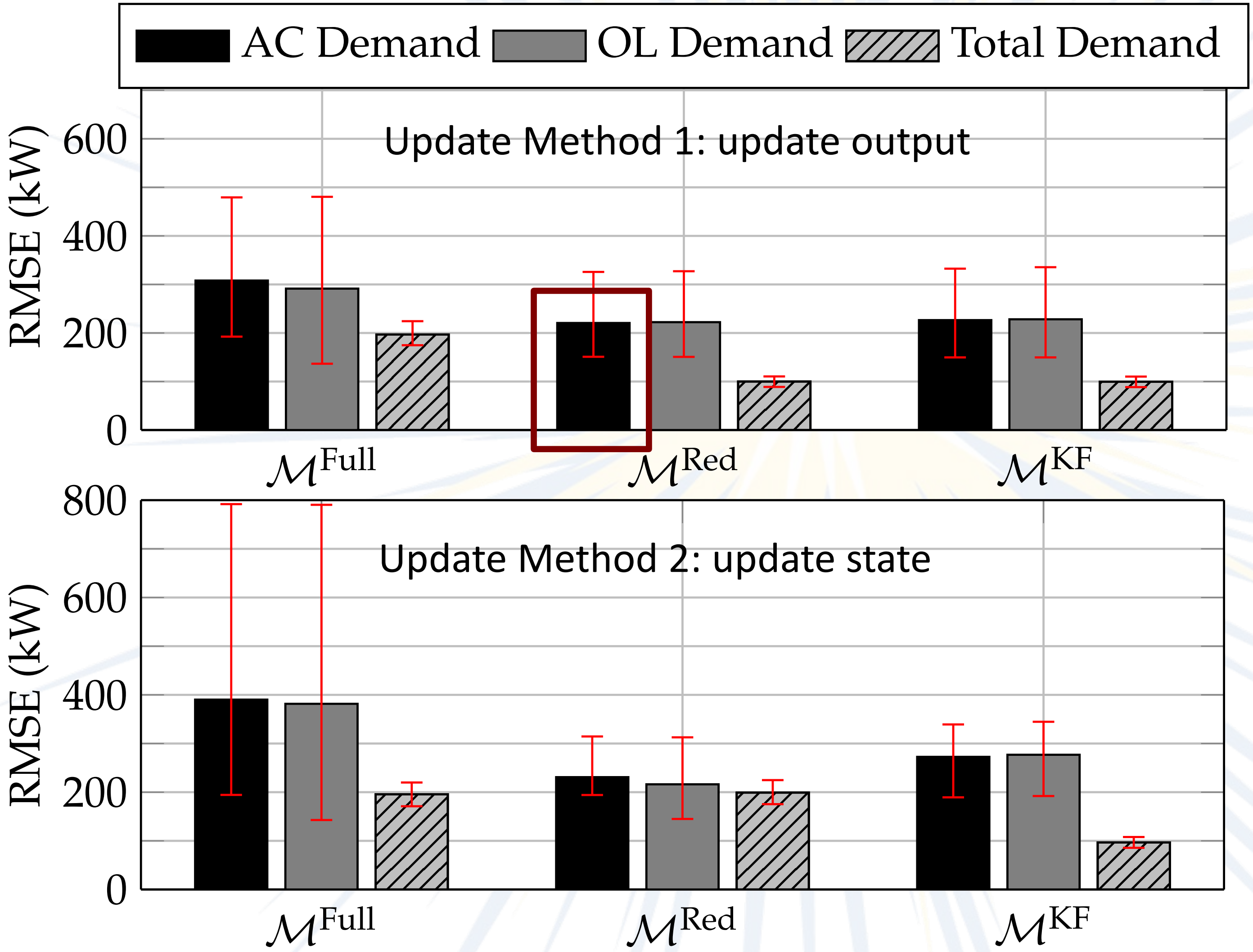
AC load RMSE

- DFS/DMD 151 kW
- BKF 177 kW
- AKF 214 kW





Comparison across model sets & update methods

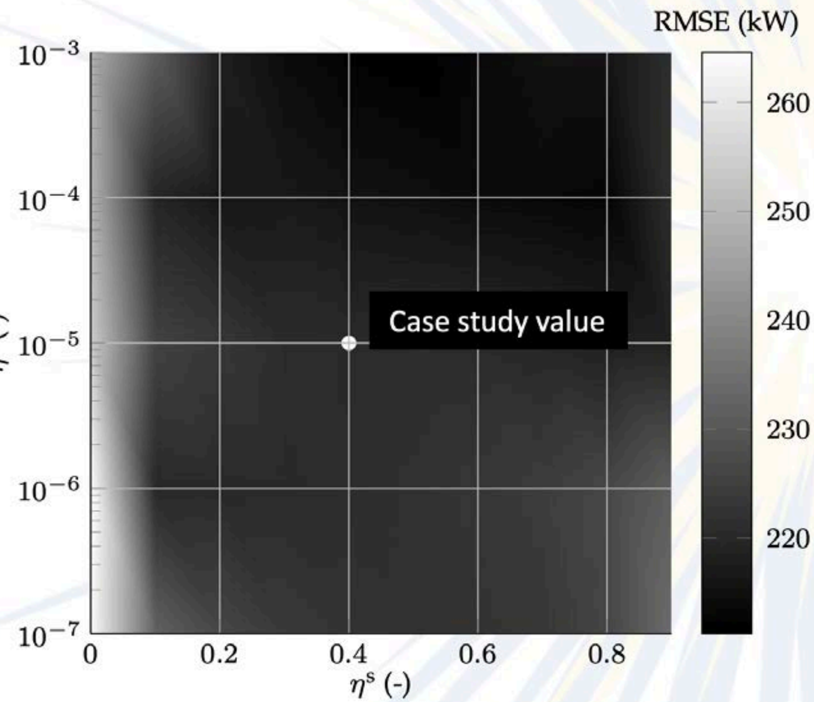


a posteriori BKF RMSE
- Mean 195 kW
- Min 148 kW
- Max 319 kW

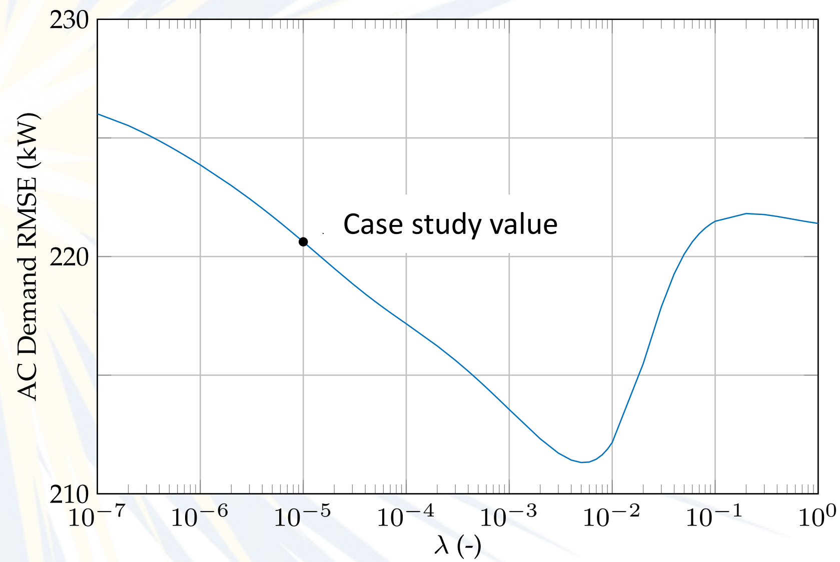
AKF RMSE
- Mean 259 kW
- Min 173 kW
- Max 358 kW

Sensitivity to parameter selections

faster transitions in weights →



larger adjustments to estimates based on prediction error →



estimate closer to the average of all models →

← a single model can dominate

Connections with Kalman Filtering

- In a Kalman Filter we assume the model form and use/choose the process and measurement noise covariance
- In DMD the model can take any form and we choose the loss and divergence functions. What should we pick?

Ledva, Du, Balzano, and Mathieu, "Disaggregating Load by Type from Distribution System Measurements in Real Time," In: Energy Markets and Responsive Grids, 2018.

Ledva, Balzano, and Mathieu, "Exploring Connections Between a Multiple Model Kalman Filter and Dynamic Fixed Share with Applications to Demand Response," IEEE CCTA 2018.

Including Error Statistics in DMD

If we make the same assumption as we make for a Kalman filter (linear model, normally distributed errors, etc.), and we choose the following loss and divergence functions

$$\ell_k(\widehat{x}_k) = \frac{1}{2}\left(C_k\widehat{x}_k - y_k\right)^T \left(\widehat{P}_k^{\mathrm{y}}\right)^{-1}\left(C_k\widehat{x}_k - y_k\right),$$

$$D\left(x\|\widehat{x}_k\right) = \tfrac{1}{2}\left(x - \widehat{x}_k\right)^T \widehat{P}_k^{-1}\left(x - \widehat{x}_k\right)$$

where $\widehat{P}_k$ and $\widehat{P}_k^{\mathrm{y}}$ are symmetric positive-definite covariance matrices corresponding to the state and output estimation error, then the DMD updates are identical to those of the Kalman filter.

Including error statistics

Use the Kalman Filter covariance update equations and compare three options for obtaining the process and measurement noise covariance

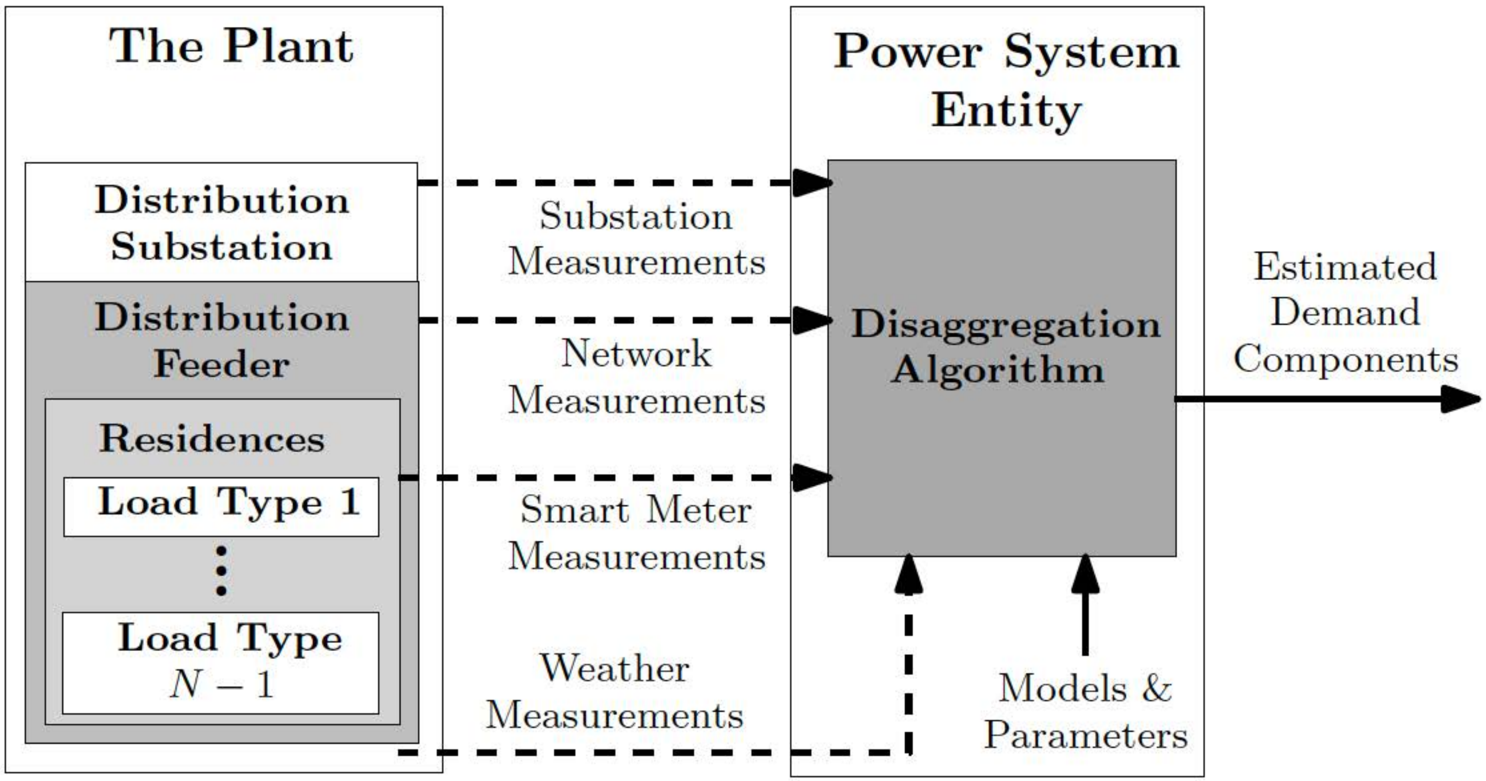
Method	Covariance	Total Demand			AC Demand			OL Demand		
		Min	Mean	Max	Min	Mean	Max	Min	Mean	Max
UM 1	Identity	88.9	100.0	110.5	151.0	220.6	325.8	150.8	222.3	327.2
UM 1	Historical	98.4	114.8	123.2	155.0	252.2	371.5	150.2	250.1	372.5
UM 1	Real-Time	146.6	154.3	168.4	120.2	125.3	131.8	104.8	114.5	130.5
UM 2	Identity	175.4	199.1	224.8	194.2	230.9	314.5	145.0	216.2	312.7
UM 2	Historical	100.5	119.5	126.1	192.0	259.8	311.5	190.6	265.5	320.2
UM 2	Real-Time	120.8	125.2	129.1	104.0	116.5	140.1	96.6	109.4	131.9
BKF	Historical	-	-	-	148.4	195.3	318.9	-	-	-
AKF	Historical	-	-	-	173.1	259.4	357.5	-	-	-

UM 1: Update Method 1 (output), UM 2: Update Method 2 (state)

DFS and Multiple Model Kalman Filtering

- We can also construct DFS to produce identical updates to a Multiple Model Kalman Filter (MMKF).
- A number of heuristics have been developed for MMKFs; these can be adapted for DFS.
  – Setting a minimum weight
  – Exponential decay used to update weights
  – Sliding window used to update weights

Multiple Measurements



Ledva and Mathieu, "Separating Feeder Demand into Components Using Substation, Feeder, and Smart Meter Measurements," IEEE Transactions on Power Systems, 2020.

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Possible Measurements

POSSIBLE REAL-TIME MEASUREMENTS

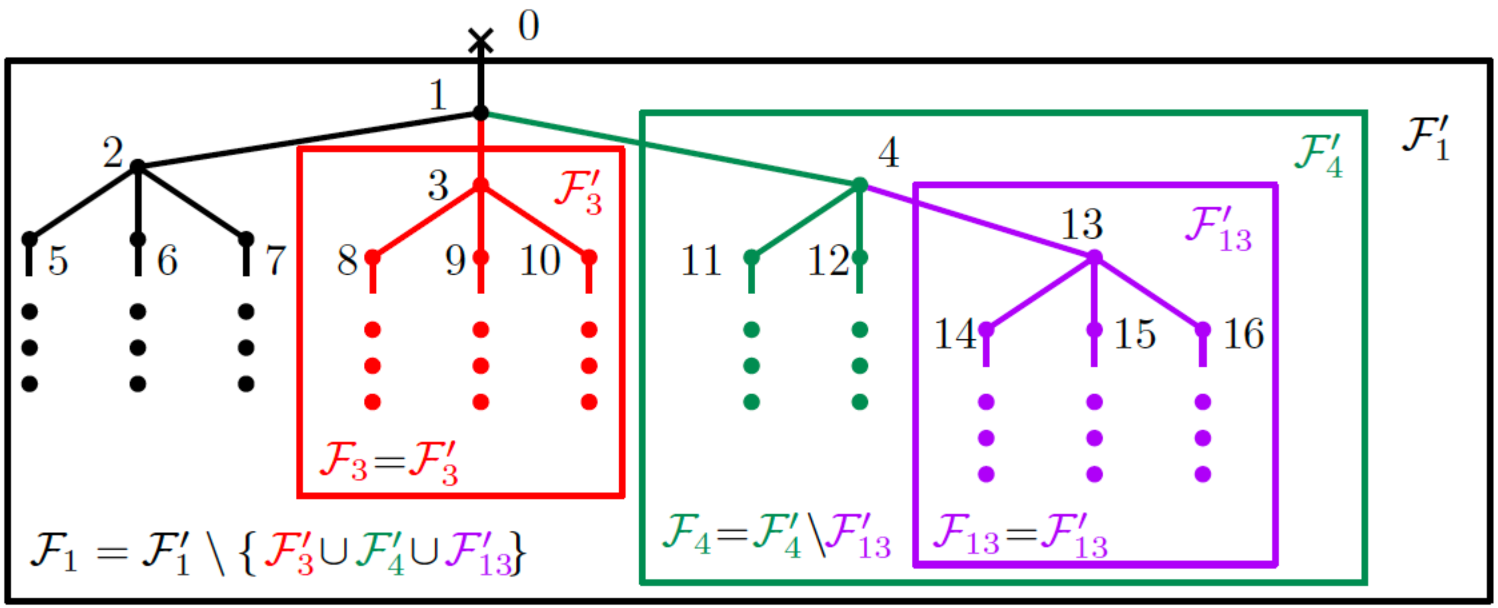
Measurement Type	Frequency
Substation Measurements	
Active and reactive power flow into the feeder	1 minute
Complex current flowing into the feeder	1 minute
Complex voltage at the feeder head	1 minute
Network Measurements	
Active and reactive power flow within the feeder	1 minute
Complex voltage within the feeder	1 minute
Smart Meter Measurements	
Active and reactive power flowing into the residence	10-60 minutes
Current magnitude flowing into the residence	10-60 minutes
Voltage magnitude at the residence	10-60 minutes
Voltage and current phase difference at the residence	10-60 minutes
Weather Measurements	
Outdoor temperature	1 minute

Approach

- Dynamic Mirror Descent ← more or less the same
- Sensor Fusion← combining different types of measurements available at different timescales
- Output equations corresponding to each type of measurement ← the hard part!
  – Real and reactive power flow from a node
  – Voltage magnitude differences
  – Voltage angle differences
  – Smart meter measurements (real/reactive power consumption)

Defining Output Equations

Feeder Portions



Output Equation

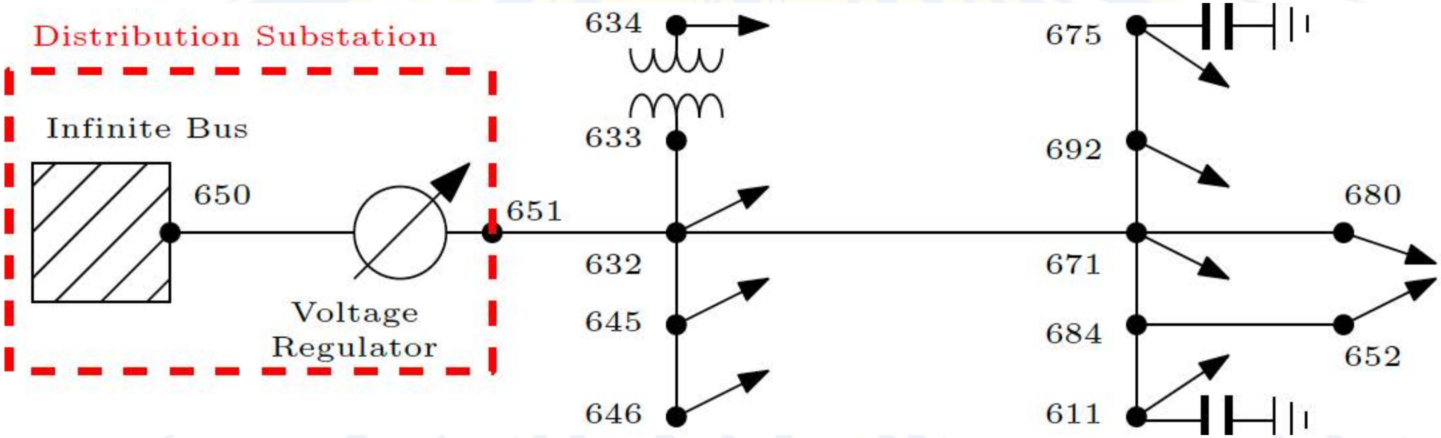
$$y = C\theta \quad \text{where} \quad \theta \triangleq \begin{bmatrix} P^{\mathrm{T}}_{\mathcal{F}_{m_1}} & \cdots & P^{\mathrm{T}}_{\mathcal{F}_{m_M}} & Q^{\mathrm{T}}_{\mathcal{F}_{m_1}} & \cdots & Q^{\mathrm{T}}_{\mathcal{F}_{m_M}} \end{bmatrix}^{\mathrm{T}},$$

y are the measurements and C depends on the measurement type

Case Study

CASE STUDY REAL-TIME MEASUREMENT SCENARIO DEFINITIONS

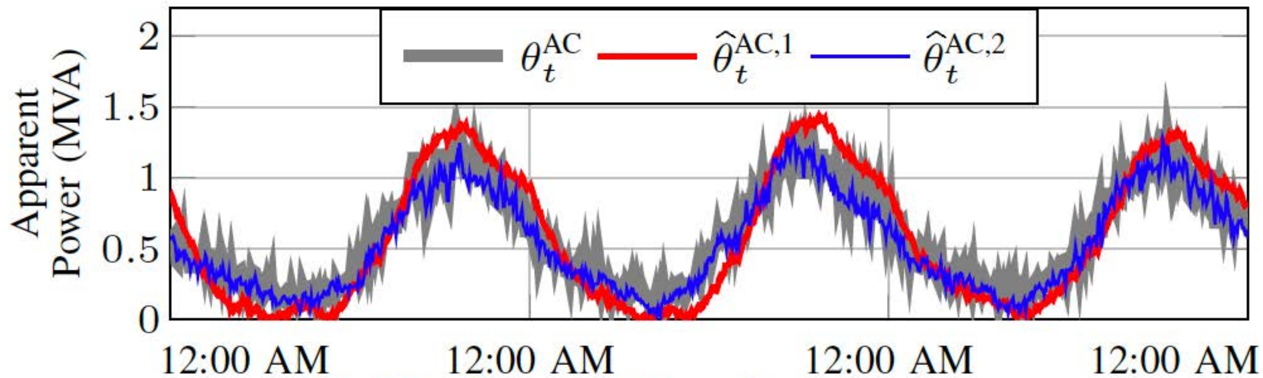
Scenario	Models	Real-Time Measurements	Purpose
1	$\mathcal{M}^{\mathrm{nc}}$	None	Evaluate the prediction accuracy of $\mathcal{M}^{\mathrm{nc}}$
2	$\mathcal{M}^{\mathrm{c}}$	Substation complex current	Evaluate the prediction accuracy of $\mathcal{M}^{\mathrm{c}}$
3	$\mathcal{M}^{\mathrm{nc}}$	Substation active power	Benchmark these results against those in [10], [11], which use a similar measurement scenario
4	$\mathcal{M}^{\mathrm{c}}$, $\mathcal{M}^{\mathrm{nc}}$	Substation apparent power; substation complex current	Evaluate the disaggregation accuracy with reactive power measurements
5	$\mathcal{M}^{\mathrm{c}}$	Scenario 4 measurements; voltage phasors at nodes 650 and 671	Evaluate the disaggregation accuracy with additional voltage phasor measurements.



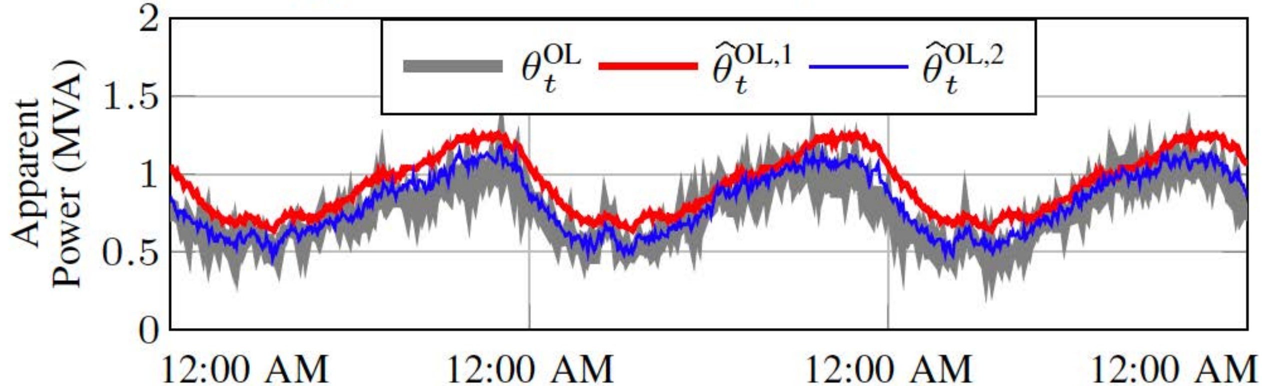
Example Results

Red = Scenario 1 (no real-time measurements)

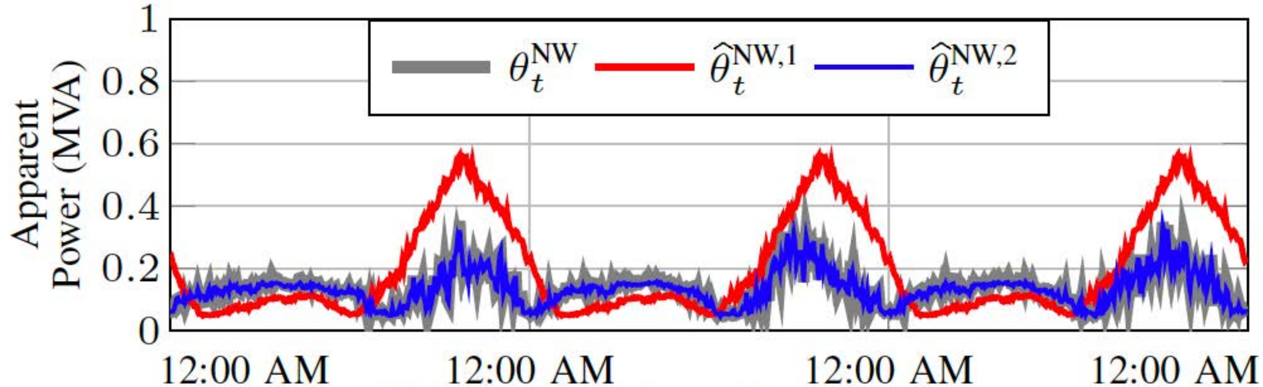
Blue = Scenario 2 (substation complex current measurement)



(a) AC Demand Time Series



(b) OL Demand Time Series



(c) NW Demand Time Series

Value of Additional Measurements

DEMAND COMPONENT RMSE (KW/KVAR/KVA) IN DIFFERENT CASES

Scenario	Models	Demand Component								
		AC-P	AC-Q	AC-S	OL-P	OL-Q	OL-S	NW-P	NW-Q	NW-S
1	$\mathcal{M}^{nc}$	181.4	45.4	187.0	179.2	52.7	186.8	50.0	157.0	165.4
2	$\mathcal{M}^{c}$	64.1	16.0	66.1	68.0	20.0	70.9	5.6	8.2	9.9
3	$\mathcal{M}^{nc}$	129.6	-	-	114.0	-	-	23.0	-	-
3-60	$\mathcal{M}^{nc}$	77.5	-	-	63.0	-	-	16.8	-	-
3-30	$\mathcal{M}^{nc}$	69.6	-	-	55.7	-	-	13.8	-	-
3-15	$\mathcal{M}^{nc}$	61.1	-	-	47.0	-	-	10.9	-	-
4	$\mathcal{M}^{nc}$	103.5	25.9	106.7	97.0	33.1	102.5	8.7	21.4	23.1
4	$\mathcal{M}^{c}$	64.1	16.0	66.1	64.8	19.6	67.7	5.7	8.2	10.0
4-60	$\mathcal{M}^{c}$	46.9	11.7	48.3	48.7	15.6	51.1	5.6	7.7	9.5
4-30	$\mathcal{M}^{c}$	45.7	11.4	47.1	47.5	14.9	49.8	5.2	7.1	8.8
4-15	$\mathcal{M}^{c}$	41.2	10.3	42.4	43.1	13.4	45.2	5.0	6.4	8.1
5	$\mathcal{M}^{c}$	61.7	15.4	63.6	62.2	20.2	65.4	6.1	13.6	15.1

Value of Additional Measurements

DEMAND COMPONENT RMSE (KW/KVAR/KVA) IN DIFFERENT CASES

Scenario	Models	Demand Component								
		AC-P	AC-Q	AC-S	OL-P	OL-Q	OL-S	NW-P	NW-Q	NW-S
1	$\mathcal{M}^{nc}$	181.4	45.4	187.0	179.2	52.7	186.8	50.0	157.0	165.4
2	$\mathcal{M}^{c}$	64.1	16.0	66.1	68.0	20.0	70.9	5.6	8.2	9.9
3	$\mathcal{M}^{nc}$	129.6	-	-	114.0	-	-	23.0	-	-
3-60	$\mathcal{M}^{nc}$	77.5	-	-	63.0	-	-	16.8	-	-
3-30	$\mathcal{M}^{nc}$	69.6	-	-	55.7	-	-	13.8	-	-
3-15	$\mathcal{M}^{nc}$	61.1	-	-	47.0	-	-	10.9	-	-
4	$\mathcal{M}^{nc}$	103.5	25.9	106.7	97.0	33.1	102.5	8.7	21.4	23.1
4	$\mathcal{M}^{c}$	64.1	16.0	66.1	64.8	19.6	67.7	5.7	8.2	10.0
4-60	$\mathcal{M}^{c}$	46.9	11.7	48.3	48.7	15.6	51.1	5.6	7.7	9.5
4-30	$\mathcal{M}^{c}$	45.7	11.4	47.1	47.5	14.9	49.8	5.2	7.1	8.8
4-15	$\mathcal{M}^{c}$	41.2	10.3	42.4	43.1	13.4	45.2	5.0	6.4	8.1
5	$\mathcal{M}^{c}$	61.7	15.4	63.6	62.2	20.2	65.4	6.1	13.6	15.1

No real-time measurements vs. complex current at substation

Value of Additional Measurements

DEMAND COMPONENT RMSE (KW/KVAR/KVA) IN DIFFERENT CASES

Scenario	Models	Demand Component								
		AC-P	AC-Q	AC-S	OL-P	OL-Q	OL-S	NW-P	NW-Q	NW-S
1	$\mathcal{M}^{nc}$	181.4	45.4	187.0	179.2	52.7	186.8	50.0	157.0	165.4
2	$\mathcal{M}^{c}$	64.1	16.0	66.1	68.0	20.0	70.9	5.6	8.2	9.9
3	$\mathcal{M}^{nc}$	129.6	-	-	114.0	-	-	23.0	-	-
3-60	$\mathcal{M}^{nc}$	77.5	-	-	63.0	-	-	16.8	-	-
3-30	$\mathcal{M}^{nc}$	69.6	-	-	55.7	-	-	13.8	-	-
3-15	$\mathcal{M}^{nc}$	61.1	-	-	47.0	-	-	10.9	-	-
4	$\mathcal{M}^{nc}$	103.5	25.9	106.7	97.0	33.1	102.5	8.7	21.4	23.1
4	$\mathcal{M}^{c}$	64.1	16.0	66.1	64.8	19.6	67.7	5.7	8.2	10.0
4-60	$\mathcal{M}^{c}$	46.9	11.7	48.3	48.7	15.6	51.1	5.6	7.7	9.5
4-30	$\mathcal{M}^{c}$	45.7	11.4	47.1	47.5	14.9	49.8	5.2	7.1	8.8
4-15	$\mathcal{M}^{c}$	41.2	10.3	42.4	43.1	13.4	45.2	5.0	6.4	8.1
5	$\mathcal{M}^{c}$	61.7	15.4	63.6	62.2	20.2	65.4	6.1	13.6	15.1

Complex current vs. real power at substation

Value of Additional Measurements

Demand Component RMSE (kW/kVar/kVA) in Different Cases

Scenario	Models	AC-P	AC-Q	AC-S	OL-P	OL-Q	OL-S	NW-P	NW-Q	NW-S
1	$\mathcal{M}^{nc}$	181.4	45.4	187.0	179.2	52.7	186.8	50.0	157.0	165.4
2	$\mathcal{M}^{c}$	64.1	16.0	66.1	68.0	20.0	70.9	5.6	8.2	9.9
3	$\mathcal{M}^{nc}$	129.6	-	-	114.0	-	-	23.0	-	-
3-60	$\mathcal{M}^{nc}$	77.5	-	-	63.0	-	-	16.8	-	-
3-30	$\mathcal{M}^{nc}$	69.6	-	-	55.7	-	-	13.8	-	-
3-15	$\mathcal{M}^{nc}$	61.1	-	-	47.0	-	-	10.9	-	-
4	$\mathcal{M}^{nc}$	103.5	25.9	106.7	97.0	33.1	102.5	8.7	21.4	23.1
4	$\mathcal{M}^{c}$	64.1	16.0	66.1	64.8	19.6	67.7	5.7	8.2	10.0
4-60	$\mathcal{M}^{c}$	46.9	11.7	48.3	48.7	15.6	51.1	5.6	7.7	9.5
4-30	$\mathcal{M}^{c}$	45.7	11.4	47.1	47.5	14.9	49.8	5.2	7.1	8.8
4-15	$\mathcal{M}^{c}$	41.2	10.3	42.4	43.1	13.4	45.2	5.0	6.4	8.1
5	$\mathcal{M}^{c}$	61.7	15.4	63.6	62.2	20.2	65.4	6.1	13.6	15.1

Value of smart meter measurements (no complex current)

Value of Additional Measurements

Demand Component RMSE (kW/kVar/kVA) in Different Cases

Scenario	Models	AC-P	AC-Q	AC-S	OL-P	OL-Q	OL-S	NW-P	NW-Q	NW-S
1	$\mathcal{M}^{nc}$	181.4	45.4	187.0	179.2	52.7	186.8	50.0	157.0	165.4
2	$\mathcal{M}^{c}$	64.1	16.0	66.1	68.0	20.0	70.9	5.6	8.2	9.9
3	$\mathcal{M}^{nc}$	129.6	-	-	114.0	-	-	23.0	-	-
3-60	$\mathcal{M}^{nc}$	77.5	-	-	63.0	-	-	16.8	-	-
3-30	$\mathcal{M}^{nc}$	69.6	-	-	55.7	-	-	13.8	-	-
3-15	$\mathcal{M}^{nc}$	61.1	-	-	47.0	-	-	10.9	-	-
4	$\mathcal{M}^{nc}$	103.5	25.9	106.7	97.0	33.1	102.5	8.7	21.4	23.1
4	$\mathcal{M}^{c}$	64.1	16.0	66.1	64.8	19.6	67.7	5.7	8.2	10.0
4-60	$\mathcal{M}^{c}$	46.9	11.7	48.3	48.7	15.6	51.1	5.6	7.7	9.5
4-30	$\mathcal{M}^{c}$	45.7	11.4	47.1	47.5	14.9	49.8	5.2	7.1	8.8
4-15	$\mathcal{M}^{c}$	41.2	10.3	42.4	43.1	13.4	45.2	5.0	6.4	8.1
5	$\mathcal{M}^{c}$	61.7	15.4	63.6	62.2	20.2	65.4	6.1	13.6	15.1

Value of smart meter measurements (with complex current)

Value of Additional Measurements

DEMAND COMPONENT RMSE (KW/KVAR/KVA) IN DIFFERENT CASES

Scenario	Models	Demand Component								
		AC-P	AC-Q	AC-S	OL-P	OL-Q	OL-S	NW-P	NW-Q	NW-S
1	$\mathcal{M}^{\mathrm{nc}}$	181.4	45.4	187.0	179.2	52.7	186.8	50.0	157.0	165.4
2	$\mathcal{M}^{\mathrm{c}}$	64.1	16.0	66.1	68.0	20.0	70.9	5.6	8.2	9.9
3	$\mathcal{M}^{\mathrm{nc}}$	129.6	-	-	114.0	-	-	23.0	-	-
3-60	$\mathcal{M}^{\mathrm{nc}}$	77.5	-	-	63.0	-	-	16.8	-	-
3-30	$\mathcal{M}^{\mathrm{nc}}$	69.6	-	-	55.7	-	-	13.8	-	-
3-15	$\mathcal{M}^{\mathrm{nc}}$	61.1	-	-	47.0	-	-	10.9	-	-
4	$\mathcal{M}^{\mathrm{nc}}$	103.5	25.9	106.7	97.0	33.1	102.5	8.7	21.4	23.1
4	$\mathcal{M}^{\mathrm{c}}$	64.1	16.0	66.1	64.8	19.6	67.7	5.7	8.2	10.0
4-60	$\mathcal{M}^{\mathrm{c}}$	46.9	11.7	48.3	48.7	15.6	51.1	5.6	7.7	9.5
4-30	$\mathcal{M}^{\mathrm{c}}$	45.7	11.4	47.1	47.5	14.9	49.8	5.2	7.1	8.8
4-15	$\mathcal{M}^{\mathrm{c}}$	41.2	10.3	42.4	43.1	13.4	45.2	5.0	6.4	8.1
5	$\mathcal{M}^{\mathrm{c}}$	61.7	15.4	63.6	62.2	20.2	65.4	6.1	13.6	15.1

Value of including complex voltage measurements

Conclusions

- Dynamic Mirror Descent (DMD) and Dynamic Fixed Share (DFS) enables us to solve the feeder energy disaggregation problem leveraging dynamical models of arbitrary form
- Empirical results are often comparable to the a posteriori best Kalman filter (obtained from the same models)
- We can leverage ideas from Kalman filtering to inform our choice of DFS functions/parameters and heuristics
- The approach extends to cases with multiple measurements
- Lastly, POWER SYSTEMS NEEDS NILM!

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